

# Time-resolved adaptive FEM simulation of the DLR-F11 aircraft model at high Reynolds number

Johan Hoffman<sup>1</sup> Johan Jansson<sup>1,2</sup> Niclas Jansson<sup>1</sup> Rodrigo Vilela de Abreu<sup>1</sup>

Computational Technology Laboratory, HPCViz, CSC, KTH [1] Basque Center for Applied Mathematics (BCAM) [2]

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## Main ingredients of our paper

### Objective

...we would like to present a new methodology for computational aerodynamics, and we would like this methodology to establish a new direction for the field.

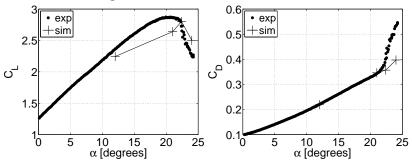
### How to achieve that? (or "Road map" to presentation)

- Show quantitatively good/excellent results.
- Present main features of the method.
- Show hard figures of computational costs.



## Key results I, lift breakdown

### Case 2b / config4 / Re=15.1M



**Fig:**  $C_L$ ,  $C_D$ , vs. angle of attack.

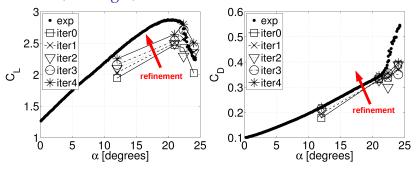
▶ Lift breakdown observed but no significant increase in drag.

**•** ...



### Key results I, lift breakdown

### Case 2b / config4 / Re=15.1M



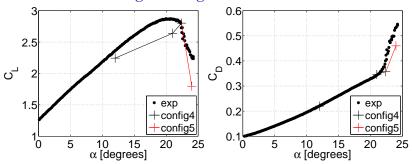
**Fig:**  $C_L$ ,  $C_D$ , vs. angle of attack.

- Lift breakdown observed but no significant increase in drag.
- ▶ Refined result "approaches" measurements.



## Key results II, stall prediction

### Case 2b+3b / config4+config5 / Re=15.1M

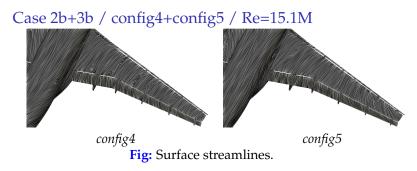


**Fig:**  $C_L$ ,  $C_D$ , vs. angle of attack.

- "config4", angle of attack  $\alpha = 12^{\circ}$ , 21° and 22.4°.
- "config5", angle of attack  $\alpha = 24$  °.
- ▶ Lift breakdown observed AND significant increase in drag for "config5", angle of attack  $\alpha = 24$ °.



### Key results II, stall prediction



- Similar patterns along the wing.
- ► Stall cells growing towards the wing tip of "config5".



## Key results, summary

### Case 2b / config4 / Re = 15.1M

- lift breakdown...
- ...BUT no clear increase in drag! Worse match to experiments...

### Case 3b / config5 / Re = 15.1M

- lift breakdown...
- ...AND clear increase in drag! Better match to experiments...

#### Conclusion

Need full geometry (config5) to correctly predict experimental results.

# Method highlights, DFS<sup>1</sup>

### The General Galerkin method (G2)

- **FEM** with piecewise linear approximation in space and time.
- ► Fully unstructured meshes.
- ► Time-resolved method where numerical stabilization based on the residual dissipates turbulent kinetic energy.
- ► Slip velocity boundary condition with small (zero) skin friction.
- ► Adaptive mesh refinement with respect to output of interest using associated adjoint problem to estimate errors in output.

<sup>&</sup>lt;sup>1</sup>Direct Finite Element Simulation



#### In other words

- ► Unstructured meshes ~ solve problems with complex geometries.
- ► Time-resolved method ~ no turbulence modeling.
- ► Slip velocity boundary condition  $\sim$  **no boudary layer mesh**.
- ► Adjoint-based adaptive mesh refinement ~ cells put on the right place, fewer cells, cheaper.

For  $\hat{U}=(U,P)$  a weak solution,  $\hat{\varphi}=(\varphi,\theta)$  a solution to a linearized adjoint problem, and  $M(\hat{U})=((\hat{U},\hat{\psi}))$  a mean value output, with  $\hat{\psi}$  a weight function, we define the error estimate:

$$|M(\hat{u}) - M(\hat{U})| = |((\hat{u} - \hat{U}, \hat{\psi}))| \leq \sum_{K \in \mathcal{T}_n} \mathcal{E}_K,$$

with the error indicator:

$$\mathcal{E}_{K} \equiv \sum_{n=1}^{N} \left[ \int_{I_{n}} |R_{1}(\hat{U})|_{K} \cdot \omega_{1} dt + \int_{I_{n}} |R_{2}(U)|_{K} \omega_{2} dt + \int_{I_{n}} |SD_{\delta}^{n}(\hat{U}; \hat{\varphi})_{K}| dt \right],$$

for each element *K* in the mesh  $\mathcal{T}_n$ , with stability weights  $\omega_i$ , i = 1, 2.

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for each element *K* in the mesh  $\mathcal{T}_n$ , with stability weights  $\omega_i$ , i = 1, 2.



### How do we generate the mesh?

#### Adaptive algorithm

- 1. For the mesh  $\mathcal{T}_n$ : compute primal and adjoint problem.
- 2. Compute error indicator for all cells
- 3. Mark 10% of the elements with highest "error indicator" for refinement.
- 4. Generate the refined mesh  $\mathcal{T}_{n+1}$ , and goto 1.

<u>Initial mesh</u> (angle of attack 12°):

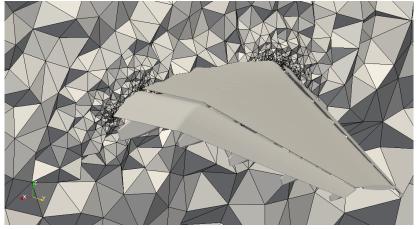
3.8M cells

<u>Final mesh</u> (after 4 adaptive refinements):

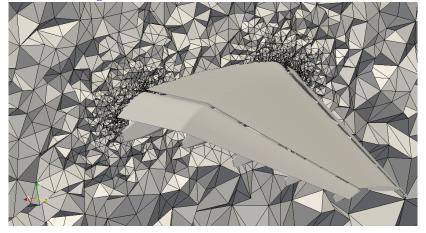
22.6M cells

 $\Rightarrow$  Compare, e.g., with committee's medium mesh, 99M cells for half airplane!

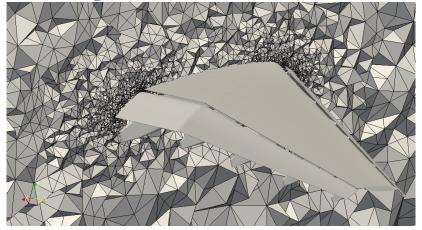




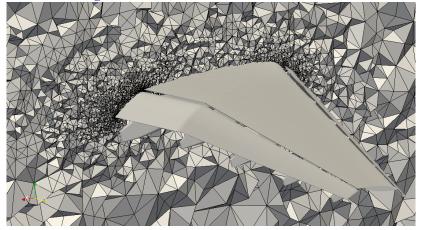




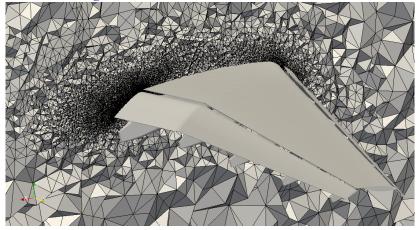






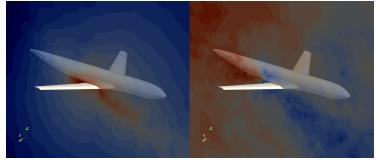








### How adjoint adaptivity works

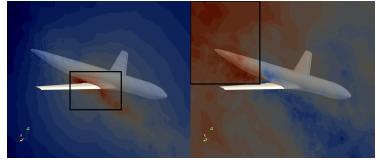


Adjoint velocity.

Momentum residual.



### How adjoint adaptivity works

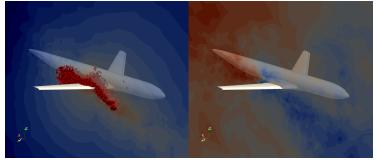


Adjoint velocity.

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### How adjoint adaptivity works



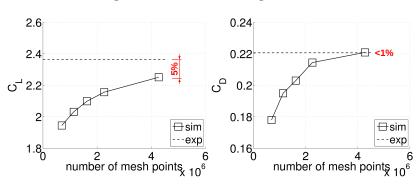
Marked cells refinement.

Adjoint velocity.



### More results, convergence

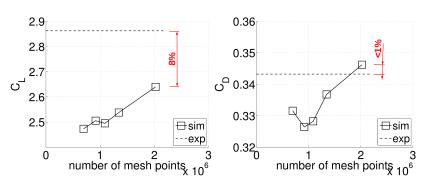
### Case 2b / config4 / Re=15.1M / Angle of attack 12 $^{\circ}$





### More results, convergence

### Case 2b / config4 / Re=15.1M / Angle of attack 21 $^{\circ}$





## Computational resources

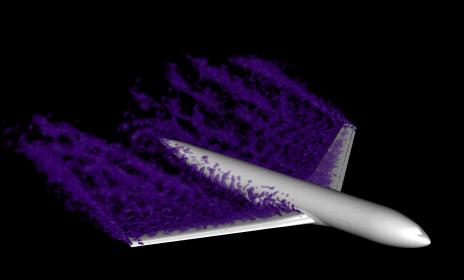
### Lindgren at PDC/KTH

- ▶ 1,516 node Cray XE6.
- Dual 12-core nodes (36,384 cores).
- ▶ 32 GB DDR3 per node.
- Cray Gemini (3-D Torus topology).



#### Simulation time

- ▶ 200,000 core hours (adaptive algorithm for 1 angle of attack).
- $\blacktriangleright$  800,000 all simulations (12 °, 21 °, 22.4 ° and 24 °.).
- ▶ Roughly 1 month on 1,000 cores.





### **Conclusions**

### We were able to compute the flow around a full aircraft model at high Re...

- ...stall prediction for config5.
- ...adaptive solution approaches experimental values.
- ...without boundary layer.
- ...with a time-dependent method.
- ...with fewer cells than anybody else.
- ...with (our own) open-source software.

#### Next, we would like to...

...perform further simulations with config5.



### Unicorn, DOLFIN @ open-source FENiCS-project

http://dryad.csc.kth.se/projects/dolfin-hpc/files http://dryad.csc.kth.se/projects/unicorn-hpc/files http://www.fenicsproject.org/

#### Acknowledgements

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